

Figure 3 Chip layout of linear AMR sensor, A: parallel curved NiFe-strips, connected in meander structure B: eight fields of meander stripes lead to two Wheatstone bridges

The assumption of having a corresponding magnetization direction in the meander strip imprinting the external magnetic field direction fails because of two reasons:

1. Anisotropic field acts against external field arising from geometric form and material properties of the meander strip [5].
2. Pinning of meander strip edge domains.

As a result, the signal contains a deviation of the expected ideal change of resistance and hysteresis behavior [6].

Using stronger magnetic fields will decrease both effects by forcing the alignment of the domains to the external field direction. A more suitable way of compensating harmonics even at lower fields is done by consciously created inverted harmonic sub-signals, which will interfere destructively. This is enhanced by the meander strip layout.

Harmonic compensation by shape of meander stripe

Using a linear AMR sensor which is placed **perpendicular** to a scale needs filtering of harmonics in the sensor signal by splitting straight parts of the meander strips into two or more groups of defined angles between the parallel directions of the meander strips.

Increasing the number of groups leads to a higher order of harmonics, which will be filtered out of the sensor signal. As a disadvantage the separation of the strip into sub-strips may lead to pinning effects on the edges between each group.

Using a curved shape for the meander stripes, leads to a continuous and simultaneous propagation of the domains. This eliminates the domain pinning effects. Finally an isotropic layout approach leads to a symmetric pattern of meander areas where no field direction is preferred. The corresponding sensor layout shows a high gain in accuracy compared to the simple flat stripe design. This is shown in figure 4.

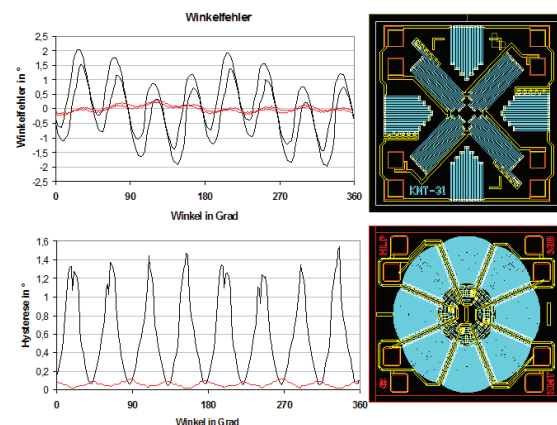


Figure 4 Performance comparison between flat and curved meander stripe design. Red: accuracy, black: hysteresis, measured at applied field strength of 8 kA/m

Example for harmonic compensation by geometrical shift of meander stripes

Looking to a sin/cos position sensor placed **in plane** on top of a magnetic scale the following way of harmonic compensation is typically used. The periodicity is 2 mm (1mm north pole, 1 mm south pole), basic frequency = f_1 .

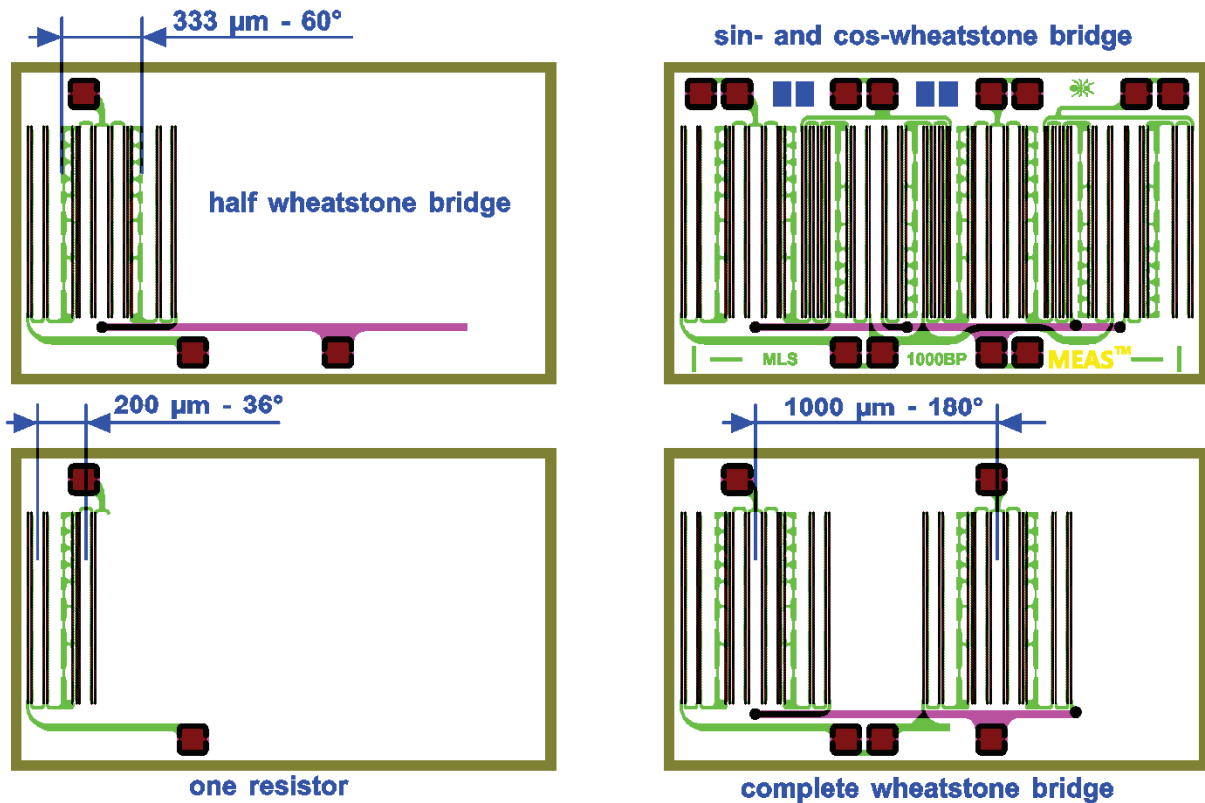


Figure 5 Chip layout of linear AMR sensor for *in plane* applications, harmonic compensation through geometrical displacement of compensation fields

One resistor contains two meander groups with a distance of 200 μm or 36° phase difference. This group eliminates the 5th harmonic. The resistors form a half Wheatstone-bridge, having a distance of 333 μm or 60° phase difference. This combination eliminates the 3th harmonic. Both half bridges are combined to a Wheatstone bridge, which have a distance of 1000 μm or 180° phase difference. This combination eliminates all even harmonics and so forth.

Modern DFN packages allow new applications

The integration of the sensor head and the scale into a mechanical system is very often restricted by space limitations.



Figure 6 Comparison between COB based chip assembly on ceramic and DFN package

Here the use of modern DFN packages in combination with new scale materials, that allow much thinner scale thickness, opens the door for new applications, where precise linear displacement measurements are needed in a very limited space.

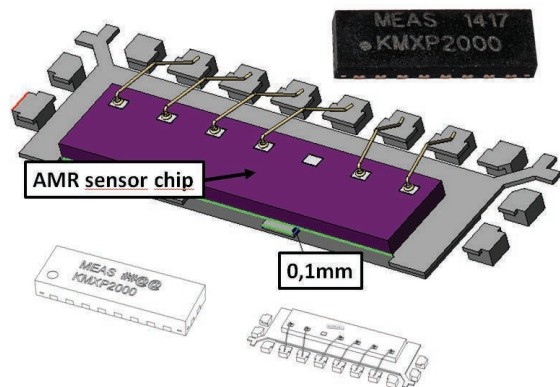


Figure 7 Assembly of KMXP series DFN packaged AMR linear sensor, maximum air gap of sensor to package edge = 0,1mm

As the sensor chip has to be placed as close as possible to the scale a typical assembly technology today is chip-on-board (COB, see figure 6)), which is a costly, non-standard assembly process. Modern DFN packages are tiny, robust and most importantly, allow standard

SMT processes. They provide much better defined mechanical tolerances as standard glob tops (see figure 7), with much less mechanical internal stress by giving a robust protection to the sensor chip and a well defined placement on the printed circuit board.

Perpendicular and flat sensor to scale alignments

The following two examples illustrate where the beneficial properties of DFN packages apply: Figure 8 shows the common application, where the sensor is placed on the edge of the PCB. DFN packages also allow a perpendicular assembly, so that the PCB can now be placed parallel to the scale. The sensor chip itself stays at perpendicular alignment to the scale.

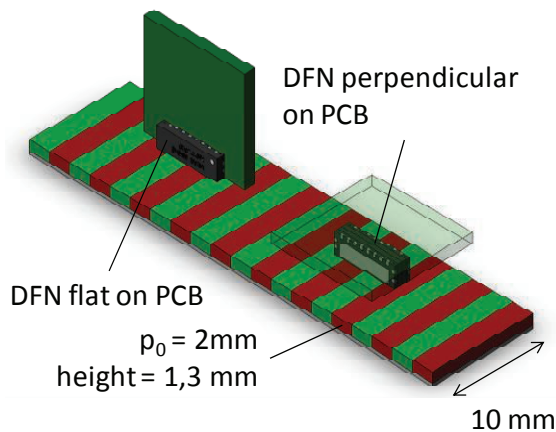


Figure 8 flat and perpendicular DFN packaged AMR sensor, air gap: 1mm @ $p_0 = 2\text{mm}$, chip alignment to scale remains perpendicular

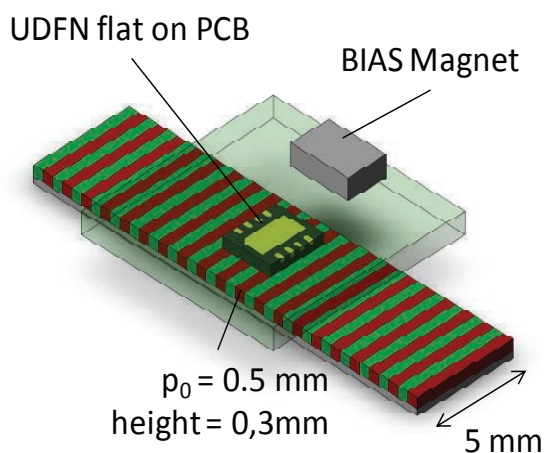


Figure 9 extra thin track (height = 0,3mm) with flat UDFN packaged MR sensor, air gap: 0,125mm @ $p_0 = 0,5\text{mm}$, flat chip alignment to scale leads to very small air gaps

For more precise measurements very small pole pitches are needed which in turn requires very small air gaps. Figure 9 depicts how this measurement task can be addressed utilizing an ultrathin DFN package.

Linear measurement systems based on DFN packaged linear AMR sensors

When designing a linear magnetic encoder one has to take 3 parameters into account:

1. Used sensor principle
2. Magnetic scale
3. Application

The overall system accuracy depends mainly on a small tolerance band of the air gap between sensor and scale as well as of the scale quality itself.

Common scale qualities ensure accuracies of $\pm 40 \mu\text{m/m}$ down to $\pm 10 \mu\text{m/m}$ [7]. This accuracy field is often reached after just some millimeter scale although it is not exceeded over 1 meter scale as defined.

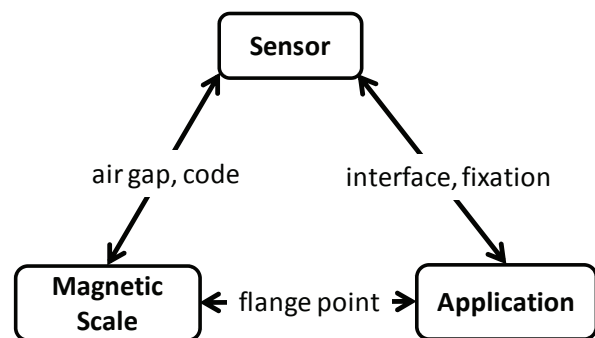


Figure 10 Triangle of Encoder design, dependencies of design parameters

Using DFN packaged linear AMR sensors enable a maximum air gap between scale and sensor as the component could be placed directly to the edge of the PCBA. The three-sided pad layout ensures exact alignment during the SMT soldering process.

As result high accurate linear encoders down to $\pm 3 \mu\text{m}$ accuracy could be generated when combined with a high accurate magnetic scale as shown in figure 11.

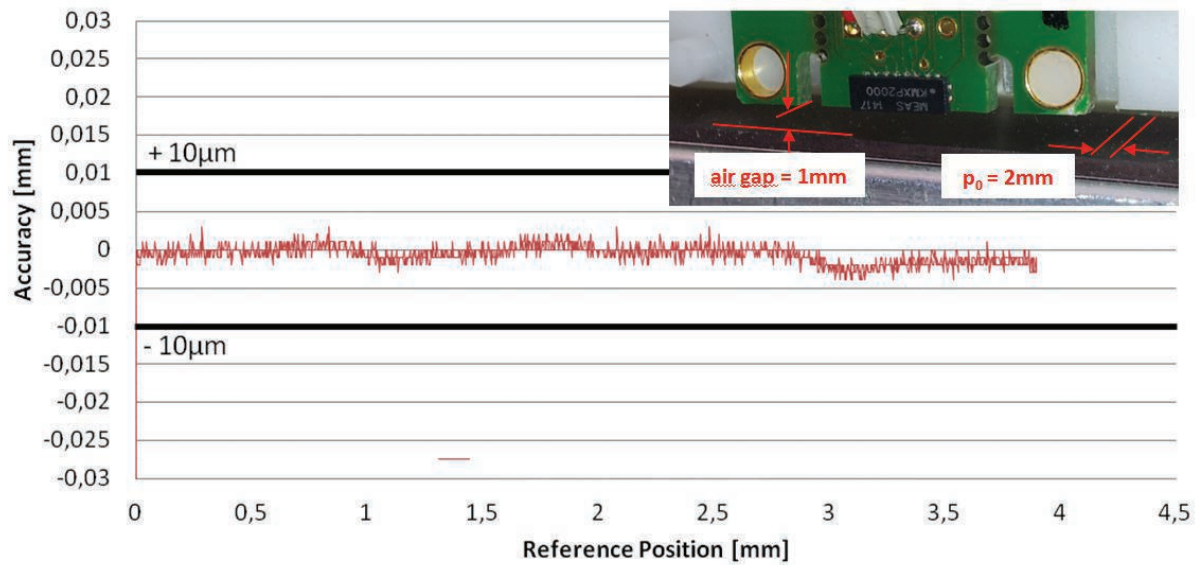


Figure 11 Accuracy plot of a flat mounted KMX2000 DFN magnetic length sensor, using pole pitch $p_0 = 2\text{mm}$

References

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